## Air-operated index table

An air signal and ratchet mechanism ensure that the table rotates at a fixed angle and fixed direction. For operation principles, see p.1331.

## Thin, lightweight, compact, and high torque

$1.0 \mathrm{~N} \cdot \mathrm{~m}[0.74 \mathrm{ft} \cdot \mathrm{lbf}]$ (At operating air pressure 0.5 MPa [73psi.])
10 times increase of allowable energy
(Compared to the previous model)


Sensor switch for operations check is optional.


Locating dowel pin holes placed on the top of the table and bottom of the body


## Two rotation directions: <br> Rotation to the right (clockwise), Rotation to the left (countericockwise)

Note: Will not rotate in reverse direction.
Three rotation angles: $45^{\circ}, 60^{\circ}$ and $90^{\circ}$


## Application example

Change the orientation of the circuit board and perform soldering.
(In combination with Creseed soldering unit)


Rotary Stage uses air signal and ratchet mechanism to ensure that the table rotates at a fixed angle and fixed direction.

| Process | Table operation | Ratchet mechanism operation | Piston portion operation |
| :---: | :---: | :---: | :---: |
| (1) Completion of table rotation | Table in secured condition. | - Knock plate pushes on stopper A to secure the gear in place. <br> - Ratchet secures the gear in place. |  |
| (2) Start of piston return |  <br> Table in secured condition. | Stopper A secures the gear in place. <br> - Ratchet releases the gear, and rotates along with the knock plate. |  |
| (3) Completion of piston return | - Table in secured condition. |  | Applying pressure <br> - Piston moves to the end of piston return side. |
| (4) Start of table rotation | Table links with piston portion and rotates. | - Ratchet uses stopper B to release stopper A from the gear. <br> Ratchet secures gear in place, and rotates along with the knock plate and gear. |  |
| (5) Completion of table rotation | - Table rotates for fixed angle, and arrives at secured position. | - Knock plate pushes on stopper A to secure the gear in place. <br> Ratchet secures the gear in place. | - Piston moves to the end of piston rotation side. |

The table is linked to the gear by pin C.
The ratchet and knock plate are located on the same plate, and move in tandem.
The ratchet is linked by a connecting shaft to the piston.
The rotary stage RWT series goes through steps (1) $\rightarrow$ (2) $\rightarrow$ (3) $\rightarrow$ (4) $\rightarrow$ (5) above to complete 1 cycle.
Notes: 1. When operating the Rotary Stage RWT series, always start from the step "(1) Completion of table rotation."
2. If the Rotary Stage RWT series stops while partway through rotation due to a drop in pressure, etc., always start from "(3) Completion of piston return."
3. When connecting the Rotary Stage RWT series to a valve, connect the normally open side to the rotation-side connection port.


## General precautions

## Media

1. Use air for the media. For the use of any other media, consult us.
2. Air used for the actuator should be clean air that contains no deteriorated compressor oil, etc. Install an air filter (filtration of a minimum $40 \mu \mathrm{~m}$ ) near the actuator or valve to remove collected liquid or dust. In addition, drain the air filter periodically.

## Piping

1. Always thoroughly blow off (use compressed air) the tubing before connecting it to the actuator. Entering metal chips, sealing tape, rust, etc., generated during piping work could result in air leaks or other defective operation.
2. When screwing piping or fittings into the actuator, tighten to the appropriate tightening torque shown below.

| Connecting thread | Tightening torque $\mathrm{N} \cdot \mathrm{cm}[\mathrm{in} \cdot \mathrm{lbf}]$ |
| :---: | :---: |
| $\mathrm{M} 5 \times 0.8$ | $157[13.9]$ |

## Lubrication

The product can be used without lubrication, if lubrication is required, use Turbine Oil Class 1 (ISO VG32) or equivalent. Avoid using spindle oil or machine oil.

## Atmosphere

If using in locations subject to dripping water, dripping oil, etc., use a cover to protect the unit. Also, avoid dew condensation.

## Operation

When starting up operations of a device and the actuator by supplying compressed air rapidly, it could not control the speed due to the construction of the actuator, resulting in damage to the device and actuator. When shutting off compressed air, shut off with the table in a completely rotated state, and check that the stopper has activated. If for some reason the compressed air is shut off while the Rotary Stage is partway through a rotation, apply air pressure through the return side connection port (PB port) and continue applying back pressure in the operation to use. (See the operating principles on p.1331.)


## Mounting

## Mounting

1. Horizontal mounting (face up on the table surface) is the only acceptable mounting direction. Any other mounting directions will cause the inner parts to disengage, resulting in damage or defective operation.

2. The mounting surface should always be flat. Twisting or bending during mounting may result in air leaks or improper operation.
3. Care should be taken that scratches or dents on the actuator's mounting surface may damage its flatness.
4. Take some locking measures when shocks or vibrations might loosen the bolts.
5. For workpiece mounting, female threads are available for installing the workpiece in place on the table. Always use bolts so that the screw length is less than the depth of the female thread. Use of longer bolts than the female thread will interfere with the inner parts, and prevent
 them from working properly. When mounting the workpiece, tighten the bolts within the range of the tightening torque.


Caution: When using a bolt to mount the workpiece in place on the table, hold either the table or the workpiece during operation. Holding the body for tightening will apply excessive moment to the stopper or gear, etc., damaging them.
6. When mounting the Rotary Stage RWT series, tighten screws applying torque within the allowable range.

Mounting using through holes on the body


| Model | Mounting | Screw size | Maximum tightening <br> torque $(\mathrm{N} \cdot \mathrm{m})[\mathrm{t} \cdot \mathrm{lbf}]$ |
| :---: | :---: | :---: | :---: |
| ARWT10 | Through hole | M5 $\times 0.8$ | $3.0[2.2]$ |

## Allowable load

| Item Model | ARWT10 |
| :--- | :---: |
| Allowable thrust load Ws $\left(\mathrm{N}[\mathrm{lbf} . \mathrm{J})^{\text {Note1 }}\right.$ | $50[11.2]$ |
| Allowable radial load $\mathrm{W}_{\mathrm{R}}\left(\mathrm{N}[\mathrm{lbf} .)^{\text {Note2 }}\right.$ | $0[0]$ |
| Allowable bending moment $\mathrm{M}(\mathrm{N} \cdot \mathrm{m}[\mathrm{ft} \cdot \mathrm{bff})$ | $1.5[1.1]$ |

Notes: 1. The thrust load has directionality. (See the diagram below.)
Do not apply it to the table surface in the up direction.
2. Cannot be used where a radial load is applied.


## Radial load



Bending moment


| $\mathrm{N} \cdot \mathrm{m}[\mathrm{ft} \cdot \mathrm{lbf}]$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Model | Air pressure MPa [psi.] |  |  |  |  |  |  |  |  |
|  | $\begin{gathered} 0.2 \\ {[29]} \\ \hline \end{gathered}$ | $\begin{aligned} & 0.25 \\ & {[36]} \\ & \hline \end{aligned}$ | $\begin{gathered} 0.3 \\ {[44]} \\ \hline \end{gathered}$ | $\begin{aligned} & 0.35 \\ & {[51]} \\ & \hline \end{aligned}$ | $\begin{gathered} 0.4 \\ {[58]} \\ \hline \end{gathered}$ | $\begin{aligned} & 0.45 \\ & {[65]} \\ & \hline \end{aligned}$ | $\begin{gathered} 0.5 \\ {[73]} \\ \hline \end{gathered}$ | $\begin{aligned} & 0.55 \\ & {[80]} \\ & \hline \end{aligned}$ | $\begin{gathered} 0.6 \\ {[87]} \\ \hline \end{gathered}$ |
| ARWT10 | $\begin{gathered} 0.4 \\ {[0.30]} \end{gathered}$ | $\begin{gathered} 0.5 \\ {[0.37]} \end{gathered}$ | $\begin{gathered} 0.6 \\ {[0.44]} \end{gathered}$ | $\begin{gathered} 0.7 \\ {[0.52]} \end{gathered}$ | $\begin{gathered} 0.8 \\ {[0.59]} \end{gathered}$ | $\begin{gathered} 0.9 \\ {[0.66]} \end{gathered}$ | $\begin{gathered} 1.0 \\ {[0.74]} \end{gathered}$ | $\begin{gathered} 1.1 \\ {[0.81]} \end{gathered}$ | $\begin{gathered} 1.2 \\ {[0.89]} \\ \hline \end{gathered}$ |



## Rotation time control

$1 \mathrm{~N} \cdot \mathrm{~m}=0.7376 \mathrm{ft} \cdot \mathrm{lbf} \quad 1 \mathrm{Mpa}=145 \mathrm{psi}$.

For control of rotation time, a sequence control using sensor switches at both stroke ends for detection is recommended.
If using timer control, caution should be exercised for the following points.

- For the rotation side, check that the rotation is completed all the way to the end point, and that the stopper positively activates.
- Because no visual check is possible for the return side, set the time to 0.2 second or more, without using a speed controller for adjustment.


## Finding the air flow rate

 (for selecting F.R.L., valves, etc.)$Q_{1}=\left(6.4 \times \frac{60}{t} \times \frac{P+0.1013}{0.1013}+200 *\right) \times 10^{-3}$
$Q_{1}{ }^{\prime}=\left(0.391 \times \frac{60}{t} \times \frac{P^{\prime}+14.696}{14.696}+12.20 *\right) \times \frac{1}{1728}$

## OFinding the air consumption

$Q_{2}=\left(v \times n \times \frac{P+0.1013}{0.1013}+200 \%\right) \times 10^{-3}$

Q1: Required air flow rate for rotary stage
Q2: Air consumption of rotary stage
V: Cylinder capacity of rotary stage per cycle
t : Time required for 1 cycle of the rotary stage
n : Number of operations per minute
P : Pressure
$\ell / m i n(A N R)$
$\ell / m i n(A N R)$
$\mathrm{cm}^{3}$
s
cycle/min
MPa
$\mathrm{Q}_{2}{ }^{\prime}=\left(\mathrm{V}^{\prime} \times \mathrm{n} \times \frac{\mathrm{P}^{\prime}+14.696}{14.696}+12.20 \%\right) \times \frac{1}{1728}$
$Q_{1}{ }^{\prime}$ : Required air flow rate for rotary stage
ft 3/min. (ANR)*
Q2': Air consumption of rotary stage ft 3/min. (ANR)*
V': Cylinder capacity of rotary stage per cycle
$t$ : Time required for 1 cycle of the rotary stage
n : Number of operations per minute
$P^{\prime}$ : Pressure
sec . cycle/min. psi.
*Refer to p .54 for an explanation of ANR.
※: The Rotary Stage RWT series may leak air when operated at less than $200 \mathrm{~cm}^{3} / \mathrm{min}[12.20 \mathrm{in} 3 / \mathrm{min}$.] (ANR), because of the cylinder structure.

Cylinder capacity of rotary stage per cycle
$\mathrm{cm}^{3}$ [in. ${ }^{3}$ ]

| Model | ARWT10-45 | ARWT10-60 | ARWT10-90 |
| :---: | :---: | :---: | :---: |
| Cylinder capacity $\mathrm{V}\left[\mathrm{V}^{\prime}\right]$ | $9.6[0.586]$ | $10.6[0.647]$ | $12.8[0.781]$ |

Note: One cycle of the Rotary stage consists of movement that returns the device to the return position in preparation for traveling the internal piston by an air signal, and sending the table as far as a fixed angle. For table rotation and piston movement, see p.1331.

Caution: For the load and rotation time, follow the below "Model selection procedure" to select within the range of specified values. Moreover, about $80 \%$ of the allowable values is recommended to use in the application. By using these values, adverse effects on cylinders and guides can be a minimum.

## OModel selection procedure

1. Check the application conditions

Check the following items (1)~(4)
(1) Rotation angle ( $45^{\circ}, 60^{\circ}$ and $90^{\circ}$ ) and rotation direction (clockwise or counterclockwise rotation).
(2) Rotation time (s)
(3) Applied pressure (MPa)
(4) Workpiece shape and materials
(5) Mounting direction (stance)

## 2. Check the rotation time

Check the rotation time in 1-(2) is within the rotation time adjustment range in the specification.

| Angle | Rotation time (s) |
| :---: | :---: |
| $45^{\circ}$ | $0.1 \sim 0.5$ |
| $60^{\circ}$ | $0.13 \sim 0.67$ |
| $90^{\circ}$ | $0.2 \sim 1.0$ |

Note: The rotation time is the value for 1 complete rotation operating smoothly with applying no load.

## 3. Check torque

Find the torque $\mathrm{T}_{\mathrm{A}}$ required for rotating the work.

| $\mathrm{T}_{\mathrm{A}}=1 \dot{\omega} \mathrm{~K}$ | $\mathrm{TA}_{\mathrm{A}}$ : Torque ( $\mathrm{N} \cdot \mathrm{m}$ ) |
| :---: | :---: |
|  | I : Mass moment of inertia ( $\mathrm{kg} \cdot \mathrm{m}^{2}$ ) |
| $\dot{\omega}=\frac{2 \theta}{t^{2}}$ | Use the formulas on p.1338~1341 to find. <br> $\dot{\omega}$ : Uniform angular acceleration (rad/s²) |
|  | K : Marginal coefficient 5 |
|  | $\theta$ : Rotation angle (rad) |
|  | $45^{\circ} \rightarrow 0.79 \mathrm{rad}$ |
|  | $60^{\circ} \rightarrow 1.05 \mathrm{rad}$ |
|  | $90^{\circ} \rightarrow 1.57 \mathrm{rad}$ |
|  | t : Rotation time (s) |

For the applied pressure checked in 1-(3) above, use the effective torque table or graph on p. 1333 to check that the required torque $T_{A}$ is obtained.

## 4. Check kinetic energy

If kinetic energy exceeds the allowable energy, the actuator could be damaged. Always ensure that the energy lies within the allowed level. For the allowable kinetic energy, see Table 1.

Finding the kinetic energy.

$$
\begin{aligned}
\mathrm{E}=\frac{1}{2} \times \mathrm{I} \times \omega^{2} \quad \mathrm{E} & : \text { Kinetic energy }(\mathrm{J}) \\
\mathrm{I}: & : \text { Mass moment of inertia }\left(\mathrm{kg} \cdot \mathrm{~m}^{2}\right) \\
& \text { Use the formulas on } \mathrm{p} .1338 \sim 1341 \\
\mathrm{t}=\frac{2 \theta}{\mathrm{t}} & \\
& \text { to find. } \\
\mathrm{E}<\mathrm{Ea} & \omega: \text { Angular velocity }(\mathrm{rad} / \mathrm{s}) \\
& \theta: \text { Rotation angle }(\mathrm{rad}) \\
& 45^{\circ} \rightarrow 0.79 \mathrm{rad} \\
& 60^{\circ} \rightarrow 1.05 \mathrm{rad} \\
& 90^{\circ} \rightarrow 1.57 \mathrm{rad} \\
& \mathrm{t}: \text { Rotation time }(\mathrm{s}) \\
\mathrm{Ea}: & \text { Allowable energy }
\end{aligned}
$$

... See Table 1.
Table 1. Allowable energy Ea

| Model | Allowable energy (J) |
| :---: | :---: |
| ARWT10 | 0.050 |

## OModel selection procedure

## 1. Check the application conditions

Check the following items (1)~(4)
(1) Rotation angle $\left(45^{\circ}, 60^{\circ}\right.$ and $\left.90^{\circ}\right)$ and rotation direction (clockwise rotation or counterclockwise rotation).
(2) Rotation time [sec.]
(3) Applied pressure [psi.]
(4) Workpiece shape and materials
(5) Mounting direction (stance)

## 2. Check the rotation time

Check the rotation time in 1-(2) is within the rotation time adjustment range in the specification.

| Angle | Rotation time [sec.] |
| :---: | :---: |
| $45^{\circ}$ | $0.1 \sim 0.5$ |
| $60^{\circ}$ | $0.13 \sim 0.67$ |
| $90^{\circ}$ | $0.2 \sim 1.0$ |

Note: The rotation time is the value for 1 complete rotation operating smoothly with applying no load.

## 3. Check torque

Find the torque $\mathrm{T}^{\prime} \mathrm{A}$ required for rotating the work.

$$
\begin{aligned}
& \left.\mathrm{T}^{\prime} \mathrm{A}=\mathrm{I}^{\prime} \dot{\omega} \mathrm{K} \quad \mathrm{~T}^{\prime} \mathrm{A}: \text { Torque [ft } \cdot \mathrm{lbf}\right] \\
& \dot{\omega}=\frac{2 \theta}{t^{2}} \quad \mathrm{I}^{\prime}: \text { Mass moment of inertia [lbf•ft•sec.2] } \\
& \dot{\omega}=\frac{2 \theta}{\mathrm{t}^{2}} \quad \text { Use the formulas on } \mathrm{p} .1338 \sim 1341 \text { to find. } \\
& \dot{\omega} \text { : Uniform angular acceleration [rad/sec.2] } \\
& \text { K : Marginal coefficient } 5 \\
& \theta \text { : Rotation angle [rad] } \\
& 45^{\circ} \rightarrow 0.79 \mathrm{rad} \\
& 60^{\circ} \rightarrow 1.05 \mathrm{rad} \\
& 90^{\circ} \rightarrow 1.57 \mathrm{rad} \\
& \mathrm{t} \text { : Rotation time [sec.] }
\end{aligned}
$$

For the applied pressure checked in 1-3 above, use the effective torque table or graph on $p .1333$ to check that the required torque T'A is obtained.

## 4. Check kinetic energy

If kinetic energy exceeds the allowable energy, the actuator could be damaged. Always ensure that the energy lies within the allowed level. For the allowable kinetic energy, see Table 1.

Finding the kinetic energy.

$$
\begin{aligned}
& E^{\prime}=\frac{1}{2} \times I^{\prime} \times \omega^{2} \\
& \mathrm{E}^{\prime} \text { : Kinetic energy [ft•lbf] } \\
& \omega=\frac{2 \theta}{t} \\
& \text { Use the formulas on p.1338~1341 } \\
& \text { to find. } \\
& \omega \text { : Angular velocity [rad/sec.] } \\
& \mathrm{E}^{\prime}<\mathrm{E}^{\prime} \mathrm{a} \\
& \theta \text { : Rotation angle [rad] } \\
& 45^{\circ} \rightarrow 0.79 \mathrm{rad} \\
& 60^{\circ} \rightarrow 1.05 \mathrm{rad} \\
& 90^{\circ} \rightarrow 1.57 \mathrm{rad} \\
& \mathrm{t} \text { : Rotation time [sec.] } \\
& \text { E'a: Allowable energy } \\
& \text {... See Table } 1 .
\end{aligned}
$$

Table 1. Allowable energy E'a

| Model | Allowable energy [ft•lbf] |
| :---: | :---: |
| ARWT10 | 0.037 |

## 5. Check load ratio

Check that the total sum of the load ratio does not exceed 1. For the allowable load, see Table 2. (For the load direction, see the allowable load on p.1333.)
$\frac{W_{s}}{W_{\text {S MAX }}}+\frac{M}{M_{\text {MAX }}} \leqq 1$
Table 2. Allowable load

| Model | Thrust load <br> $W_{\text {max }}(\mathrm{N})$ | Moment <br> $\mathrm{M}_{\operatorname{MAX}}(\mathrm{N} \cdot \mathrm{m})$ |
| :---: | :---: | :---: |
| ARWT10 | 50 | 1.5 |

## 6. Judgement whether the unit is usable or not

The unit is usable if it satisfies both 4 . Kinetic energy and 5 . Load ratio.

E < Ea
Total sum of load ratio $\leqq 1$

## 5. Check load ratio

Check that the total sum of the load ratio does not exceed 1.
For the allowable load, see Table 2. (For the load direction, see the allowable load on p.1333.)

$$
\frac{W^{\prime} s}{W^{\prime} s \operatorname{mAX}}+\frac{M^{\prime}}{M^{\prime} \text { mAX }^{\prime}} \leqq 1
$$

Table 2. Allowable load

| Model | Thrust load <br> W's max [lbf.] | Moment <br> M'max $[\mathrm{ft} \cdot \mathrm{bf}]$ |
| :---: | :---: | :---: |
| ARWT10 | 11.2 | 1.1 |

## 6. Judgement whether the unit is usable or not

The unit is usable if it satisfies both 4 . Kinetic energy and 5. Load ratio.
$\mathrm{E}^{\prime}<\mathrm{E}^{\prime} \mathrm{a}$
Total sum of load ratio $\leqq 1$

## Calculation example

If solid circular cylinder workpiece is on the base.
(Unit: mm)


1. Check the application conditions
(1) Rotation angle: $90^{\circ}$
(2) Rotation time: 0.5 (s)
(3) Applied pressure: 0.5 (MPa)
(4) Workpiece shape $\cdots$ as shown in the above

Workpiece materials
...Base: Aluminum alloy A5056
(Specific gravityNote $=2.64 \times 10^{3} \mathrm{~kg} / \mathrm{m}^{3}$ )
...Solid circular cylinder: Aluminum alloy A5056
(Specific gravityNote $=2.64 \times 10^{3} \mathrm{~kg} / \mathrm{m}^{3}$ )
(5) Mounting direction (stance): Horizontal

Note: Since the specific gravity can vary depending on the alloy, check the specific gravity of the metal being used, and then perform the calculation.

## 2. Check the rotation time

The rotation time is $0.5 \mathrm{~s} / 90^{\circ}$, which is within the range of $0.2 \sim 1.0 \mathrm{~s} / 90^{\circ}$, and satisfactory.

## 3. Check torque

Firstly calculate the mass moment of inertia.
Base
$m_{1}=\frac{\pi}{4} \times 0.08^{2} \times 0.01 \times 2.64 \times 10^{3}=0.133(\mathrm{~kg})$
$\mathrm{I}_{1}=\frac{0.133 \times 0.08^{2}}{8}$

$$
=1.06 \times 10^{-4}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right) \cdots(1)
$$

Solid circular cylinder

$$
\begin{aligned}
\mathrm{m}_{2} & =\frac{\pi}{4} \times 0.03^{2} \times 0.02 \times 2.64 \times 10^{3}=0.037(\mathrm{~kg}) \\
\mathrm{I}_{2} & =\frac{0.037 \times 0.03^{2}}{8}+0.037 \times 0.03^{2} \\
& =0.37 \times 10^{-4}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right) \cdots(2)
\end{aligned}
$$

From (1) and (2), the total mass moment of inertia I is
$\mathrm{I}=\mathrm{I}_{1}+\mathrm{I}_{2}$
$=1.06 \times 10^{-4}+0.37 \times 10^{-4}$
$=1.43 \times 10^{-4}\left(\mathrm{~kg} \cdot \mathrm{~m}^{2}\right) \cdots(3)$
From the given conditions, $\theta=90^{\circ}, \mathrm{t}=0.5$ (s)
Therefore, uniform angular acceleration $\dot{\omega}$ is
$\dot{\omega}=\frac{2 \times 1.57}{0.5^{2}}=12.56\left(\mathrm{rad} / \mathrm{s}^{2}\right) \cdots(4)$
From (3) and (4), the required torque $T_{A}$ is
$\mathrm{T}_{\mathrm{A}}=1.43 \times 10^{-4} \times 12.56 \times 5$

$$
=0.009(\mathrm{~N} \cdot \mathrm{~m}) \cdots(5)
$$

The effective torque at 0.5 MPa is $1.0(\mathrm{~N} \cdot \mathrm{~m})$, and the torque is satisfactory.

## Calculation example

If solid circular cylinder
base.
(Unit: in.)


1. Check the application conditions
(1) Rotation angle: $90^{\circ}$
(2) Rotation time: 0.5 [sec.]
(3) Applied pressure: 73 [psi.]
(4) Workpiece shape $\cdots$ as shown in the above

Workpiece materials
...Base: Aluminum alloy A5056
[Specific gravityNote=165lbf/ft.3]
...Solid circular cylinder: Aluminum alloy A5056 [Specific gravity ${ }^{\text {Note }}=165 \mathrm{lbf} / \mathrm{ft}$.3]
(5) Mounting direction (stance): Horizontal

Note: Since the specific gravity can vary depending on the alloy, check the specific gravity of the metal being used, and then perform the calculation.

## 2. Check the rotation time

The rotation time is $0.5 \mathrm{sec} . / 90^{\circ}$, which is within the range of $0.2 \sim 1.0 \mathrm{sec} . / 90^{\circ}$, and satisfactory.

## 3. Check torque

Firstly calculate the mass moment of inertia.

## Base

$W^{\prime}{ }_{1}=\frac{\pi}{4} \times\left(\frac{3.15}{12}\right)^{2} \times\left(\frac{0.39}{12}\right) \times 165=0.290$ [lbf.]

$$
\begin{aligned}
\mathrm{l}^{\prime} & =\frac{0.290 \times(3.15 / 12)^{2}}{8 \times 32.2} \\
& =7.76 \times 10^{-5}[\mathrm{lbf} \cdot \mathrm{ft} \cdot \mathrm{sec} 2] \cdots(1)
\end{aligned}
$$

Solid circular cylinder
$W^{\prime}=\frac{\pi}{4} \times\left(\frac{1.18}{12}\right)^{2} \times\left(\frac{0.79}{12}\right) \times 165=0.082$ [lbf.]
$\mathrm{I}^{\prime}=\frac{0.082 \times(1.18 / 12)^{2}}{8 \times 32.2}+\frac{0.082 \times(1.18 / 12)^{2}}{32.2}$
$=2.77 \times 10^{-5}\left[\mathrm{lbf} \cdot \mathrm{ft} \cdot \mathrm{sec}{ }^{2}\right] \cdots(2)$
From (1) and (2), the total mass moment of inertia I' is
$I^{\prime}=I_{1}^{\prime}+I^{\prime} 2$

$$
\begin{aligned}
& =7.76 \times 10^{-5}+2.77 \times 10^{-5} \\
& \left.=1.05 \times 10^{-4}\left[\mathrm{lbf} \cdot \mathrm{ft} \cdot \mathrm{sec}^{2}\right]\right] \cdots(3)
\end{aligned}
$$

From the given conditions, $\theta=90^{\circ}, \mathrm{t}=0.5$ [sec.]
Therefore, uniform angular acceleration $\dot{\omega}$ is
$\dot{\omega}=\frac{2 \times 1.57}{0.5^{2}}=12.56[\mathrm{rad} / \mathrm{sec} .2] \cdots(4)$
From (3) and (4), the required torque $\mathrm{T}^{\prime} \mathrm{A}$ is
$\mathrm{T}^{\prime} \mathrm{A}=1.05 \times 10^{-4} \times 12.56 \times 5$

$$
=0.0066[\mathrm{ft} \cdot \mathrm{lbf}] \cdots(5)
$$

The effective torque at 73 psi . is 0.74 [ $\mathrm{ft} \cdot \mathrm{lbf}$ ], and the torque is satisfactory.

## 4．Check kinetic energy

From the given conditions，$\theta=90^{\circ}, \mathrm{t}=0.5$（s）
Therefore，

$$
\omega=\frac{2 \times 1.57}{0.5}=6.28(\mathrm{rad} / \mathrm{s}) \cdots(1)
$$

From（1），kinetic energy $E$ is
$E=\frac{1}{2} \times 1.43 \times 10^{-4} \times 6.28^{2}=0.003(\mathrm{~J}) \cdots(2)$
The allowable energy is $0.050(\mathrm{~J})$ ，and the kinetic energy is satisfactory．

## 5．Check load ratio

［Thrust load】
Total mass is
$0.133+0.037=0.170(\mathrm{~kg})$
Therefore，
$W_{s}=0.170 \times 9.8=1.666(\mathrm{~N}) \cdots(1)$
［Moment】
Moment $\mathrm{M}_{1}$ of the base is
$M_{1}=0.133 \times 9.8 \times 0=0(N \cdot m) \cdots(2)$
Moment $\mathrm{M}_{2}$ of the solid circular cylinder is
$\mathrm{M}_{2}=0.037 \times 9.8 \times 0.03=0.011(\mathrm{~N} \cdot \mathrm{~m}) \cdots(3)$
From（2）and（3），the total moment is
$\mathrm{M}=0+0.011=0.011(\mathrm{~N} \cdot \mathrm{~m}) \cdots(4)$

From（1）and（4），find the load ratio．
$\frac{W_{s}}{W_{S ~ M A X}}+\frac{M}{M_{\text {MAX }}}=\frac{1.666}{50}+\frac{0.011}{1.5}=0.04<1.0$
The load ratio is less than 1．0，and satisfactory．

## 6．Judgement whether the unit is usable or not

Since kinetic energy and load ratio are both satisfied，the application is allowable．

## 4．Check kinetic energy

From the given conditions，$\theta=90^{\circ}, \mathrm{t}=0.5$［sec．］
Therefore，
$\omega=\frac{2 \times 1.57}{0.5}=6.28[\mathrm{rad} / \mathrm{sec}.] \cdots(1)$
From（1），kinetic energy $\mathrm{E}^{\prime}$ is
$\mathrm{E}^{\prime}=\frac{1}{2} \times 1.02 \times 10^{-4} \times 6.28^{2}=0.002[\mathrm{ft} \cdot \mathrm{lbf}] \cdots(2)$
The allowable energy is 0.037 ［ $\mathrm{ft} \cdot \mathrm{lbf}]$ ，and the kinetic energy is satisfactory．

5．Check load ratio
［Thrust load】
Total weight is
$0.290+0.082=0.372$［lbf．］
Therefore，
W＇s $=0.372[\mathrm{lbf}.] \cdots$（1）

## ［Moment］

Moment $\mathrm{M}^{\prime}$ of the base is
$M^{\prime}{ }_{1}=0.290 \times 0=0[\mathrm{ft} \cdot \mathrm{lbf}] \cdots$（2）
Moment $\mathrm{M}^{\prime} 2$ of the solid circular cylinder is
$\mathrm{M}^{\prime}=0.082 \times\left(\frac{1.18}{12}\right)=0.008[\mathrm{ft} \cdot \mathrm{lbf}] \cdots$（3）
From（2）and（3），the total moment is
$\mathrm{M}^{\prime}=0+0.008=0.008[\mathrm{ft} \cdot \mathrm{lbf}] \cdots$（4）
From（1）and（4），find the load ratio．
$\frac{\mathrm{W}^{\prime} \mathrm{s}}{\mathrm{W}^{\prime} \mathrm{sAX}}+\frac{\mathrm{M}^{\prime}}{\mathrm{M}^{\prime} \text { мAX }}=\frac{0.373}{11.2}+\frac{0.008}{1.1}=0.04<1.0$
The load ratio is less than 1．0，and satisfactory．
6．Judgement whether the unit is usable or not
Since kinetic energy and load ratio are both satisfied，the application is allowable．

Diagram for calculating mass moment of inertia
［When the rotation axis passes through the workpiece］
$\begin{array}{lr}\text { ODiameter } & d[\mathrm{ft} .] \\ \text { OWeight } & w[\mathrm{lbf} .]\end{array}$
d（m） m（kg）
d［ft．］


Rotating radius
$\square$
Mass moment of inertia I＇［lbf•ft•sec．？］
Rotating radius

| $\frac{\mathrm{d}^{2}}{8}$ |
| :--- |

$\square$

## Stepped disk


ODiameter
－Mass di portion
d2 portion
－Diameter
OWeight
di portion dz portion

Remark：For sliding use，see separate materials．
$\mathrm{d}_{1}(\mathrm{~m})$ Mass moment of inertia $\mathrm{I}\left(\mathrm{kg} \cdot \mathrm{m}^{2}\right)$
$\mathrm{d}_{2}(\mathrm{~m})$ $\square$ $\mathrm{m}_{2}(\mathrm{~kg})$
$\mathrm{m}_{1}$（kg）

Rotating radius
$\square$
$\mathrm{d}_{1}$［ft．］ $\mathrm{d}_{2}[\mathrm{ft}$.
$\mathrm{w}_{1}$［lbf．］ $\mathrm{w}_{2}$［bf．］

■Mass moment of inertia $\mathrm{I}^{\prime}$［lbf•ft•sec．2］


Rotating radius

$$
\frac{\mathrm{d}_{1}{ }^{2}+\mathrm{d}_{2}{ }^{2}}{8}
$$

Remark：The $\mathrm{d}_{2}$ portion can be negligible when it is much smaller than the $\mathrm{d}_{1}$ portion．

## －Bar（rotation center is at the edge）


－Bar length
$\ell(\mathrm{m})$
－Mass moment of inertia I（kg•m²）
OMass m（kg）
Rotating radius

$\square$

| －Bar length | $\ell$［ft．］ | ■Mass moment of inertia I＇［lbf•ft sec？］ | Rotating radius |
| :---: | :---: | :---: | :---: |
| －Weight | w［lbf．］ | $I^{\prime}=\frac{w \ell^{2}}{3 \times 32.2}$ | $\frac{\ell^{2}}{3}$ |

## －Slender rod



| ORod length | $\ell 1$（m） | ■Mass moment of inertial（ $\mathrm{kg} \cdot \mathrm{m}^{2}$ ） | Rotating radius |
| :---: | :---: | :---: | :---: |
| OMass | $\begin{array}{r} \ell_{2}(\mathrm{~m}) \\ \mathrm{m}_{1}(\mathrm{~kg}) \end{array}$ | $\mathrm{I}=\frac{\mathrm{m}_{1} \ell_{1}{ }^{2}}{3}+\frac{\mathrm{m}_{2} \ell_{2}{ }^{2}}{3}$ | $\frac{\ell_{1}{ }^{2}+\ell_{2}{ }^{2}}{3}$ |
| ORod length | $\ell 1$［ft．］ | ■Mass moment of inertia I＇［lbf•ft sec．2］ | Rotating radius |
| OWeight | $\ell_{2}[\mathrm{ft}$ ．］ <br> $\mathrm{w}_{1}$［lbf．］ <br> w2［lbf．］ | $I^{\prime}=\frac{W_{1} \ell_{1}{ }^{2}}{3 \times 32.2}+\frac{W_{2} \ell_{2}{ }^{2}}{3 \times 32.2}$ | $\frac{\ell 1^{2}+\ell 2^{2}}{3}$ |

## -Bar (rotation center is through the center of gravity)

| $\rightarrow$ Bar length | $\ell(\mathrm{m})$ | $\square$ Mass moment of inertia I (kg $\cdot \mathrm{m}^{2}$ ) | Rotating radius |
| :---: | :---: | :---: | :---: |
| Mass | m (kg) | $\mathrm{I}=\frac{\mathrm{m} \ell^{2}}{12}$ | $\frac{\ell^{2}}{12}$ |
| - Bar length | $\ell$ [ft.] | $\square$ Mass moment of inertia $\mathrm{I}^{\prime}$ [ $\mathrm{lbf} \cdot \mathrm{ft} \cdot \mathrm{sec}$.] $]$ | Rotating radius |
| Weight | w [lbf.] | $I^{\prime}=\frac{w ~ ~^{2}}{12 \times 32.2}$ | $\frac{\ell^{2}}{12}$ |

## OThin rectangular plate (rectangular solid)


-Rectangular parallelepiped


Remark: For sliding use, see separate materials.

## OConcentrated load

Shape of concentrated load

| $\square$ Mass moment of inertia I $\left(\mathrm{kg} \cdot \mathrm{m}^{2}\right)$ |
| :---: |
| $\mathrm{I}=\mathrm{m}_{1} \mathrm{k}^{2}+\mathrm{m}_{1} \ell_{1}{ }^{2}+\frac{\mathrm{m}_{2} \ell_{2}{ }^{2}}{3}$ |

Rotating radius: $\mathrm{k}^{2}$ is calculated according to shape of the concentrated load.
Remark: When $\mathrm{m}_{2}$ is much smaller than $\mathrm{m}_{1}$, calculate as $\mathrm{m}_{2}=0$.
$\square$ Mass moment of inertia I' [lbf•ft•sec.]
$I^{\prime}=\frac{W_{1} k^{2}}{32.2}+\frac{W_{1} \ell_{1}{ }^{2}}{32.2}+\frac{W_{2}}{32.2} \times \frac{\ell_{2}{ }^{2}}{3}$
Rotating radius: $\mathrm{k}^{2}$ is calculated according to shape of the concentrated load.
Remark: When $w_{2}$ is much smaller than $w_{1}$, calculate as $\mathrm{w}_{2}=0$.

Gear Equation for calculating the load JL with respect to Rotary Stage axis when transmitted by gears


Gear Rotary Stage side | a |
| :---: |
| Load side |

| b |
| :--- |

Inertia moment of load
$\square$ Mass moment of inertia I (kg•m²)
Mass moment of inertia of load with respect to Rotary Stage axis
$N \cdot m$


Mass moment of inertia I' [lbf•ft•sec.2] Mass moment of inertia of load with respect to Rotary Stage axis $\mathrm{ft} \cdot \mathrm{lbf}$

## ORectangular parallelepiped

|  | Length of side | h (m) | ■Mass moment of inertia I (kg $\mathrm{m}^{2}$ ) |
| :---: | :---: | :---: | :---: |
|  | Distance from rotatio <br> Mass | $\begin{gathered} \mathrm{L}(\mathrm{~m}) \\ \mathrm{m}(\mathrm{~kg}) \end{gathered}$ | $\mathrm{I}=\frac{\mathrm{mh}^{2}}{12}+\mathrm{mL}^{2}$ |
|  | Length of side | h [ft.] | Mass moment of inertia $\mathrm{I}^{\prime}$ [lbff $\mathrm{ft} \cdot \mathrm{sec}$ ? ${ }^{\text {] }}$ |
|  | Distance from rotatio | L [ft.] | $w^{2}{ }^{2}+\mathrm{wL}^{2}$ |
|  | Weight | w [lbf.] | $=\frac{1}{32.2 \times 12}+\frac{1}{32.2}$ |

Remark: Same for cube.

## OHollow rectangular parallelepiped



Remark: Cross-section is square only.

## -Circular cylinder



| - Diameter | d (m) |
| :---: | :---: |
| - Distance from rotation axis to the center of load | L (m) |
| -Mass | m (kg) |
| - Diameter | $\mathrm{d}[\mathrm{ft}$ ] |
| - Distance from rotation axis to the center of load | L [ft.] |
| -Weight | [lbf |

Mass moment of inertia I (kg•m²)
$\square$

Mass moment of inertia I' $\left[\mathrm{lbf} \cdot \mathrm{ft} \cdot \mathrm{sec}^{2}\right.$.]
$I^{\prime}=\frac{w^{2}}{32.2 \times 16}+\frac{w L^{2}}{32.2}$

## OHollow circular cylinder



Mass moment of inertia l ( $\mathrm{kg} \cdot \mathrm{m}^{2}$ )

Mass moment of inertia $\mathrm{I}^{\prime}[\mathrm{lbf} \cdot \mathrm{ft} \cdot \mathrm{sec}$ ? $]$
$I^{\prime}=\frac{w\left(d_{2}{ }^{2}+d_{1}{ }^{2}\right)}{32.2 \times 16}+\frac{\mathrm{wL}^{2}}{32.2}$

## ROTARY STAGE

## RWT Series

## Symbol



Specifications

| Item Model | ARWT10-45-R | ARWT10-45-L | ARWT10-60-R | ARWT10-60-L | ARWT10-90-R | ARWT10-90-L |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operation type | Double acting piston type (Gear and ratchet mechanism) |  |  |  |  |  |
| Effective torque ${ }^{\text {Note1 }} \mathrm{N} \cdot \mathrm{m}[\mathrm{ft} \cdot \mathrm{lbf}]$ | 1.0 [0.74] |  |  |  |  |  |
| Media | Air |  |  |  |  |  |
| Operating pressure range MPa [psi.] | $0.2 \sim 0.6$ [29~87] |  |  |  |  |  |
| Proof pressure $\quad \mathrm{MPa}$ [psi.] | 0.9 [131] |  |  |  |  |  |
| Operating temperature range ${ }^{\circ} \mathrm{C}$ [ $\left.{ }^{\circ} \mathrm{F}\right]$ | 0~60 [32~140] (Dew condensation prohibited) |  |  |  |  |  |
| Rotation direction | Clockwise | Counterclockwise | Clockwise | Counterclockwise | Clockwise | Counterclockwise |
| Rotation angle | $45^{\circ} \pm 0.2^{\circ}$ |  | $60^{\circ} \pm 0.2^{\circ}$ |  | $90^{\circ} \pm 0.2^{\circ}$ |  |
| Rotation time adjustment range ${ }^{\text {Note } 2} \mathrm{~s} / 90^{\circ}$ | $0.2 \sim 1.0$ |  |  |  |  |  |
| Allowable energy $\quad \mathrm{J}$ [ft $\cdot \mathrm{lbf}]$ | 0.050 [0.037] |  |  |  |  |  |
| Allowable thrust load N [lbf.] | 50 [11.2] |  |  |  |  |  |
| Allowable moment $\mathrm{N} \cdot \mathrm{m}[\mathrm{ft} \cdot \mathrm{lbf}]$ | 1.5 [1.1] |  |  |  |  |  |
| Lubrication | Not required (If lubrication is required, use Turbine Oil Class 1 [ISO VG32] or equivalent.) |  |  |  |  |  |
| Port size | M5 $\times 0.8$ |  |  |  |  |  |

Notes: 1. Effective torque is the value obtained when the pressure is 0.5 MPa [73psi.].
2. The rotation time adjustment range is the value for one complete rotation operating smoothly with applying no load.

Mass

|  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Model | ARWT10-45-R | ARWT10-45-L | ARWT10-60-R | ARWT10-60-L | ARWT10-90-R | ARWT10-90-L |
| Body | $473[16.68]$ | $472[16.65]$ | $470[16.58]$ |  |  |  |
| Sensor switch AssyNote | $30[1.06]$ |  |  |  |  |  |

Note: Mass for 1 sensor switch Assy set (including 3m [118in.] cable)
Order Codes

[^0]

Note: The diagrams show the -R type (clockwise rotation). The -L type (counterclockwise rotation) is left-right symmetry.

Major Parts and Materials

| No. | Parts | Materials |
| :---: | :---: | :---: |
| $(1)$ | Body A | Aluminum alloy (anodized) |
| $(2)$ | Body B | Aluminum alloy (anodized) |
| $(3)$ | Table | Aluminum alloy (anodized) |
| $(4)$ | Base A | Stainless steel |
| $(5)$ | Swing plate | Stainless steel |
| $(6)$ | Index plate | Steel |
| $(7)$ | Knock plate | Steel |
| $(8)$ | Cover | Stainless steel |
| $(9)$ | Ratchet | Steel |
| 10 | Cam | Steel |
| $(11)$ | Pawl | Steel |
| $(12)$ | Roller | Steel |
| $(13)$ | Stopper A | Steel |
| $(14)$ | Stopper B | Steel |
| $(15)$ | Stopper C | Steel |
| $(16)$ | Main shaft | Steel |
| $(17)$ | Connecting shaft | Steel |
| $(18$ | Piston | Plastic |


| No. | Parts | Materials |
| :---: | :---: | :---: |
| (19) | Retainer | Plastic |
| (20) | Separator | Plastic |
| (21) | Gear | Steel |
| (22) | Bumper | Synthetic rubber (Urethane) |
| (23) | Clutch | - |
| (24) | Bushing A | Brass |
| (25) | Bushing B | Brass |
| (26) | Bushing D | Brass |
| (27) | Bushing E | Brass |
| (28) | Connecting pin | Stainless steel |
| (29) | Pin C | Stainless steel |
| (30) | Nut | Stainless steel |
| (31) | Spring | Stainless steel |
| (32) | Piston seal | Synthetic rubber (NBR) |
| (33) | O-ring | Synthetic rubber (NBR) |
| (34) | Hexagon socket head bolt | Stainless steel |
| (35) | Hexagon socket head bolt | Stainless steel |

ARWT10- $\square$-R-Sensor switch Assy


ARWT10- $\square$-L- Sensor switch Assy


## SENSOR SWITCH

## Specifications

| Item Model |  | SW-ARWT |
| :---: | :---: | :---: |
| Maximum detection distance ${ }^{\text {Note } 1}$ |  | 0.8 mm .] $\pm 15 \%$ |
| Stable detection range ${ }^{\text {Note } 2}$ |  | $0 \sim 0.6 \mathrm{~mm}$ [0~0.024in.] |
| Standard detected object |  | Steel $5 \times 5 \times$ t1mm [0.20×0.20 $\times 0.04$ (thickness) in.] |
| Response differential (Hysteresis) |  | $15 \%$ or less of operating distance |
| Repeatability |  | $20 \mu \mathrm{~m}$ or less |
| Voltage |  | 12~24V DC $\pm 10 \%$ Ripple P-P 10\% or less |
| Consumption current |  | 15 mA or less |
| Output |  |  |
| Output (operation) |  | Switches ON upon approach |
| Maximum response frequency |  | 1 kHz |
| Indicator lamp |  | Red LED (Lights up when output is ON) |
| Environmental resistance | Protective structure | IP67 (IEC), Watertight type (JIS) ${ }^{\text {Note } 3}$ |
|  | Ambient temperature | $-25 \sim 70^{\circ} \mathrm{C}\left[-13 \sim 158^{\circ} \mathrm{F}\right]$, in storage: $-25 \sim 80^{\circ} \mathrm{C}\left[-13 \sim 176^{\circ} \mathrm{F}\right]$ |
|  | Ambient humidity | 35~95\%RH, in storage: 35~95\%RH |
|  | Dielectric strength | AC500V 1 minute (Between every charging portion and case) |
|  | Insulation resistance | $5 \mathrm{M} \Omega$ or more at DC250V megger (Between every charging portion and case) |
|  | Vibration resistance | $10 \sim 55 \mathrm{~Hz}$ Total amplitude 1.5mm .] 2 hours for each $\mathrm{X}, \mathrm{Y}$, and Z direction (De-energized) |
|  | Shock resistance | $200 \mathrm{~m} / \mathrm{s}^{2}$ (approx. 20G) 10 times for each X, Y, and Z direction (De-energized) |
| Variation of detection distance | Temperature characteristics | Within $\pm 20 \%$ of detection distance at $20^{\circ} \mathrm{C}$ [ $68^{\circ} \mathrm{F}$ ], in ambient temperature $-25 \sim 70^{\circ} \mathrm{C}$ [ $-13 \sim 158^{\circ} \mathrm{F}$ ]. |
|  | Voltage characteristics | Within $\pm 2 \%$ when operating voltage variation is $\pm 10 \%$. |
| Materials |  | Case: stainless steel (SUS304), Plastic portion: TPX |
| Cable |  | $0.08 \mathrm{~mm}^{2}$ [1.24×10-4in.2] 3-lead Oil-resistant, heat-resistant, cold-resistant, with cabtyre cable 3m .] |
| Mass |  | Approximately 30 g [1.06oz.] |

Notes: 1. Maximum detection distance refers to the maximum detection distance for standard detected object.
2. Stable detection range refers to the distance range at which stable detection of a standard detected object is obtained, with consideration for ambient temperature and variations in supply voltage.
3. While protective structure is prescribed the sensor switch including the cable, the end of the cable is not treated to be waterproof, and therefore cannot be a target for protective structure.
For this reason, avoid applications where there is a possibility that water could intrude through the end of the cable.

## Caution

## Use in combinations with devices of the Rotary Stage RWT series only.

The sensor switch Assy (SW-ARWT) is designed to be used in combination with the Rotary Stage RWT series. Use in combination with other actuators could cause abnormal operation.

## Order Code

## SW - ARWT <br> Series <br> ARWT: Alpha series Rotary Stage RWT series

 screw)

Notes: 1. Do not loosen the setscrew. Changing the protruding length from the sensor switch holder could result in damage or defective operations.
2. When re-tightening the setscrew, check the protruding length from the holder, and fasten at a tightening torque of $0.29 \mathrm{~N} \cdot \mathrm{~m}[2.6 \mathrm{in} \cdot \mathrm{lbf}]$ $\pm 10 \%$ at a direction perpendicular to the indicator lamp.
3. One mounting pan screw ( $\mathrm{M} 3 \times 0.5$ length 8 ) is included in the sensor switch.

## Internal Circuit Diagrams



## Code $\cdots \mathrm{D}:$ Reverse current protection diode <br> Zo: Zener diode for surge voltage protection <br> Tr: NPN output transistor

## Mounting Sensor Switch

Tighten the mounting pan screw with a tightening torque of $0.63 \mathrm{~N} \cdot \mathrm{~m}[5.6 \mathrm{in} \cdot \mathrm{lbf}]$.



[^0]:    ARWT 10 $\square$ - $\square$ = $\square$

    Sensor switch Assy
    Blank: No sensor switch Assy
    SW1: With 1 set of sensor switch Assy
    SW2: With 2 sets of sensor switch Assy
    For details of sensor switch Assy, see p. 1345 and p.1346.

    ## Rotation direction

    R: Clockwise rotation
    L: Counterclockwise rotation
    Rotation angle (Number of indexing)
    45: $45^{\circ}$ (Number of indexing: 8)
    60: $60^{\circ}$ (Number of indexing: 6)
    90: $90^{\circ}$ (Number of indexing: 4)
    Nominal torque
    10: $1.0 \mathrm{~N} \cdot \mathrm{~m}[0.74 \mathrm{ft} \cdot \mathrm{lbf}]$ (At $0.5 \mathrm{MPa}[73 \mathrm{psi}$.$] pressure)$

    ## Alpha series

    Rotary Stage RWT series

